# Design of Multi-Output DC-DC Converter for Electric Vehicle Application

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# ABSTRACT

Multiport converters are essential in a range of applications, including portable electronic devices and electric vehicles (EVs). Numerous configurations of single-input multi-output (SIMO) converters have been explored in existing literature. However, these SIMO converters often face limitations such as constraints on duty cycle and inductor charging, as well as issues with cross-regulation. This work introduces a novel SIMO topology designed to overcome these limitations. The innovative design generates three distinct output voltages without imposing constraints on duty cycle or inductor currents, providing greater operational flexibility. Additionally, the design ensures effective isolation of loads during control, enhancing overall system performance and reliability.

#### **1. INTRODUCTION**

In the past decade, there has been a growing demand for renewable energy sources in applications such as electric vehicles (EVs), auxiliary power, and grid-connected systems. Multiport DC-DC converters are crucial in these applications as they hybridize energy sources, reducing the number of components, system complexity, and overall cost compared to using multiple separate single-input DC-DC converters [1-3].

Several Multiport Converter (MPC) designs have been introduced over the past decade. A notable SIMO converter proposed generates boost, buck, and inverted outputs simultaneously; each controlled independently [4]. However, this design requires n + 2 switches to produce 'n' voltage levels, increasing the converter's size and cost. Issues in calculating state-space equations and output voltages for the SIMO converter] were addressed and rectified [5].

A single coupled inductor-based SIMO buck converter offers less output inductor current ripple compared to single inductor SIMO converters [6]. Nayak and Nath provided a detailed

comparison of Single Input Dual Output (SIDO) converters using coupled inductors versus single inductors, highlighting that coupled inductor SIDO converters exhibit better steady-state and transient performance. However, in single inductor SIMO configurations, the inductor is switched between the loads, which can lead to cross-coupling issues [7].

Various control approaches have been proposed in the literature to address the crossregulation issue in single inductor-based SIMO converters. Current predictor controller is introduced in [8], which replaces the conventional charge-balance method. Although effective, generating duty ratios for the active switches with this method is quite complex. Deadbeat-based control method relies on an output current observer. This method, however, is sensitive to noise and significant parametric variations [9].

A SIMO converter using a multivariable digital controller is proposed to minimize voltage ripples, suppress cross-regulation issues, and regulate output voltages. While effective, this controller design can increase the system's overall complexity.

A non-isolated, single-switch SIMO converter topology featuring fewer components and reduced system cost is introduced [10]. However, regulating the outputs independently poses a challenge. To address the issues in single inductor SIMO converters, non-isolated SIMO converters have been proposed [11], which independently regulate output voltages without requiring an additional control circuit.

A high gain step-up and SEPIC converter-based SIMO configuration is suggested for PV applications [12-15]. This setup provides outputs higher than the supply voltage and enhances output voltage with additional capacitors and diodes, although it increases cost and conduction losses.

However, these systems exhibit lack of load isolation during operation. Additionally, grounding issues can arise when charging the battery with simultaneously active loads, increasing circuit complexity for converting one of the negative output voltages into buckboost mode. To overcome these issues, the proposed converter is modeled with multi output.

#### 2. METHODOLOGY

Figure 1(a) illustrates a proposed DC-DC configuration with a single input and three output channels. This configuration includes several key components: an input voltage source labelled as  $V_{DC}$ , switches (S<sub>1</sub>-S<sub>3</sub>), diodes (D<sub>1</sub>-D<sub>3</sub>), and passive elements (L<sub>1</sub>-C<sub>1</sub>, L<sub>2</sub>-C<sub>2</sub>, and L<sub>3</sub>-C<sub>3</sub>). Its primary function is to generate three distinct output voltages: a

boost voltage ( $V_{01}$ ), a buck-boost voltage ( $V_{02}$ ) with a positive polarity, and a buck voltage ( $V_{03}$ ).



FIGURE 1a. Proposed configuration

This versatile converter is well-suited for the independent regulation of the output voltages using the duty cycles  $D_1$ ,  $D_2$ , and  $D_3$ , respectively.



FIGURE 1b. Theoretical waveforms.

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Figure 1b provides a visual representation of the theoretical waveforms of the circuit elements, offering insights into their dynamic behavior and performance characteristics. The proposed circuit configuration significantly differs from the conventional parallel combination of buck, boost, and buck-boost converters. In the proposed design, load isolation is achieved during simultaneous control. This control strategy ensures that all loads remain isolated from each other, regardless of the operational mode. Such load isolation is not achievable in conventional parallel combination of buck, boost converters. Although this circuit configuration may appear simple, it introduces a novel and valuable approach.

### 2.1 Operating stages



FIGURE 2. Operating states: (a) Switching state-1 and (b) Switching State-2.

Mode-1 Operation (Figure 2(a)):

- Only load R<sub>3</sub> is connected to the input power supply through switch S<sub>3</sub>.
- All other loads are intentionally isolated from the power supply.

Mode-2 Operation (Figure 2 (b)):

- Only load R<sub>1</sub> is connected to the input supply via diode D<sub>1</sub>.
- Again, all other loads are deliberately isolated from the power supply.

# Switching state 1

Switches  $S_1$ ,  $S_2$ , and  $S_3$  are in the ON position, establishing the current flow path as illustrated in Figure 2(a). This configuration results in the activation of energy ports  $V_{DC}$ , causing inductors  $L_1$ ,  $L_2$ , and  $L_3$  to become magnetized. As a consequence, capacitors  $C_1$  and  $C_2$  discharge their stored energy to supply power to the respective loads represented by  $R_1$  and  $R_2$ . Simultaneously, capacitor  $C_3$  undergoes a charging process.

# Switching state 2

In this state,  $L_1$ ,  $L_2$ ; and  $L_3$  are de-magnetized and deliver their energy to the load through  $D_1$ ,  $D_2$  and  $D_3$ , respectively.

# **3. RESULTS AND DISCUSSION**

The model has been built in MATLAB environment to verify the proposed system with  $V_{DC}$  50 V, frequency is 50 kHz, and the duty ratio is 50%. The parameter details are as follows,

# Table 1

# **Simulation Parameters**

Parameter	Simulation	
Input voltage(V <sub>DC</sub> )	50 V	
Output voltage(v <sub>01</sub> /v <sub>02</sub> /v <sub>03</sub> )	100/50/25 V	
Output currents(I <sub>01</sub> /I <sub>02</sub> /I <sub>03</sub> )	2/2/2 A	
Switching frequency(f)	50kHz	
Inductor( $L_1/L_2/L_3$ )	0.6/0.9/1 mH	
Capacitor( $C_1/C_2/C_3$ )	200/470/360 uF	

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The corresponding output voltages ( $V_{01}$ ,  $V_{02}$ , and  $V_{03}$ ) are illustrated in Figure 4.1(a-c), respectively.







(c) buck-boost configurations

The results demonstrate that the proposed configuration generates stable, independent output voltages that are unaffected by sudden changes in supply.

# 4. COMPARATIVE ANALYSIS

The comparison of the proposed converter with a conventional SIMO converter in terms of several key factors, as summarized in Table 2 below.

<b>TABLE 2.</b> Comparison betwee	n the conventional and	proposed SIMO converter.
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Comparison different aspects	Conventional	Proposed
Number of components	6	6
Output voltage	Buck, Boost and Buck-	Buck, Boost and Buck-
	Boost(Negative output	Boost(Positive output
	voltage)	voltage)
Inverting circuit is required	Yes	No
for the positive output		
voltage		
Loads are isolated to each	No	Yes
other during control		

This comparison highlights the advantages of the proposed SIMO converter in terms of reduced component count, lower circuit complexity, and effective handling of cross-regulation, among other factors.

### **5. CONCLUSION**

This work introduces a novel SIMO (Single Input Multiple Output) converter architecture, thoroughly explaining its operational principles and modes. The proposed configuration is notable for its simplicity, as it operates without assumptions regarding inductor charging or operating duty cycles. This versatility allows it to generate output voltages in buck, boost, and buck-boost configurations, all with independent voltage regulation. Importantly, the topology effectively ensures that sudden variations in inductor and load currents do not adversely impact the output voltages. To validate its functionality and performance, the paper presents simulation results, demonstrating the efficacy of the proposed converter design.

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